



Resonant rf network antennas for inductively-coupled plasma sources

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Introduction

Resonant rf networks are new plasma sources with numerous potential applications in plasma processing [1]. They consist of parallel arrangements of **L**, **C** elementary meshes with resonant frequencies corresponding to the normal modes for the current/voltage distributions. At each resonant frequency, very high currents are generated in the antenna structure, hence it can be used as an inductively-coupled plasma source (ICP).

Experimental setup

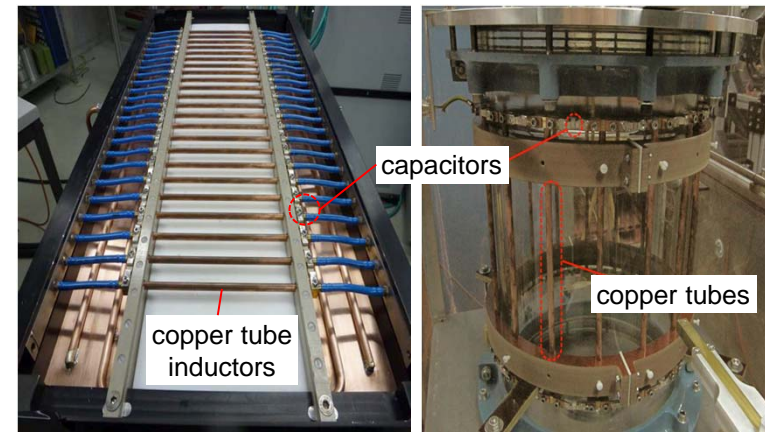


Fig. 1: Left: 23-leg planar resonant network before it is embedded in a dielectric and placed inside a vacuum chamber. Right: 16-leg cylindrical (birdcage) resonant antenna. The vacuum vessel is a glass cylinder closed at top and bottom by grounded metal plates.

The planar antenna in Figs. 1, 2 is for large area surface treatment; the cylindrical antenna is for volume plasma sources. The **N** parallel legs of each antenna are made of copper tubes which act as inductive elements **L**. High Q capacitors **C** link the legs together and present a small inductance **M**.

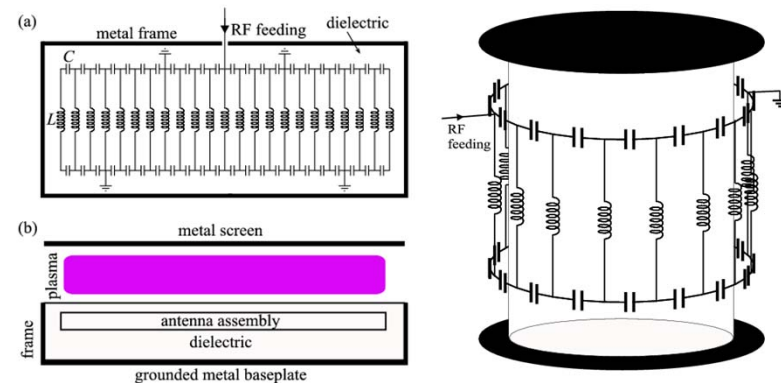


Fig. 2: Left: Schematic of a 23-leg planar rf network antenna. (a) Top view; (b) Side view showing the metal screen used to confine the plasma.

Right: Schematic of a 16-leg cylindrical (birdcage) rf antenna, showing the points of rf feeding and grounding.

Solving Kirchhoff's equations with the boundary conditions of the planar structure gives $m = [1, \dots, N-1]$ normal modes [2]. Each mode has a specific current distribution (Fig. 3) and a resonance frequency

$$f_m = \frac{1}{2\pi} [C(M - 2L \sin^2\{\frac{m\pi}{2N}\})]^{-1/2}.$$

Mutual impedances must be accounted for to reproduce the measured frequencies. The antenna behaves as a **R**, **L**, **C** parallel resonance circuit for each mode [2].

These plasmas show an *E-H* transition similar to ICP devices using solenoids or spiral coils [3]. Resonant rf networks have a real impedance near resonance which avoids strong voltages or currents in the rf power feedline, regardless of network size.

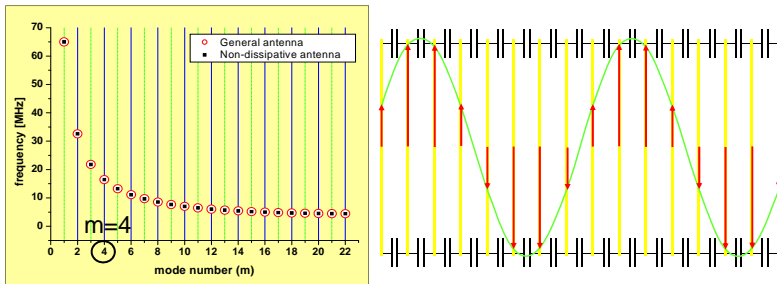


Fig. 3: Left: The mode frequencies of the planar antenna. The frequencies are not strongly altered by power dissipation in the antenna. Right: Current distribution in the planar antenna legs for mode $m = 4$.

Prototypes of Helyssen antennas operating at 13.56 MHz have been tested up to 2 kW rf power and are currently under industrial pilot tests for barrier layer coatings in packaging, silicon thin film deposition for photovoltaic solar cells, and plasma sources for neutral beam heating.

Whistler-wave heated discharges using a planar antenna

Wave heated regimes are obtained with a static magnetic field perpendicular to the source plane above a given threshold. The measured propagating wave has the characteristics of whistler waves: The transverse magnetic field in Fig. 4 has a helical structure due to an elliptical polarization, with damped propagation away from the antenna. The high efficiency of planar resonant rf networks for launching whistler-wave heated discharges [4] means that plasma generation is not limited to a small skin-depth region, in contrast to ICP sources.

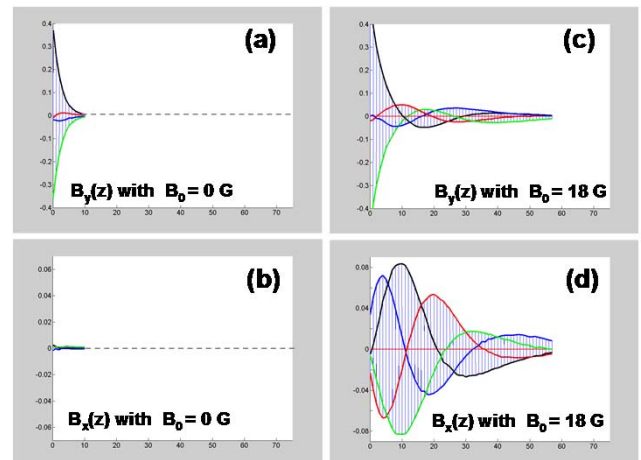


Fig. 4: Measured transverse field profile, $B_x(z)$, $B_y(z)$ along the antenna axis for quarters of a period. (a), (b) without magnetic field (inductive coupling); (c), (d) with a 18 G static magnetic field.

Conclusions

These results show the proof of principle of a novel generic type of plasma source which overcomes many of the physical and technical limitations of conventional large-area capacitive and inductive plasma sources. The general principle of resonant networks for plasma sources opens up a rich field of study, and many new permutations of plasma source physics could evolve from this concept.

Acknowledgments

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References

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